



AS BUILD DOCUMENTATION

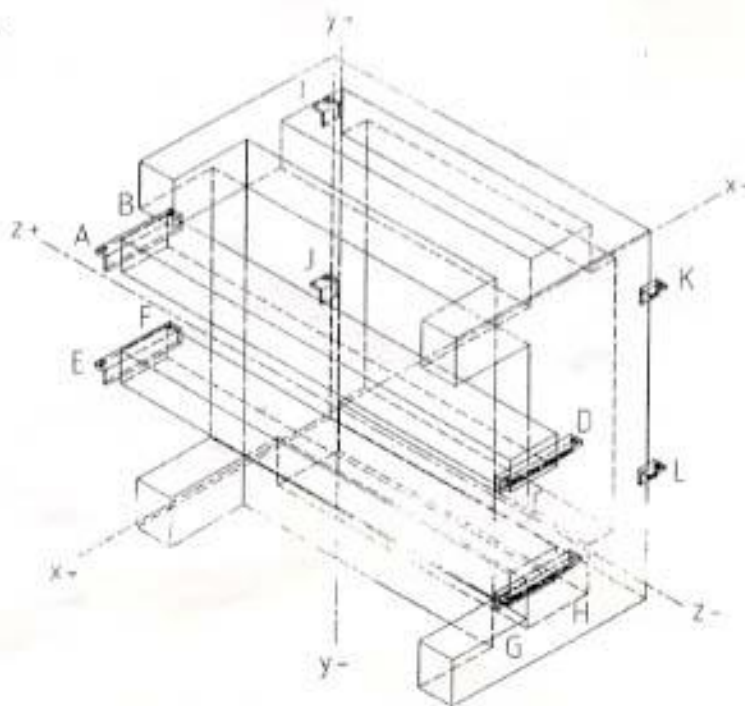
SCI3IDI

7.2. TABLES AND GRAPHS FOR BL4 WIGGLER.

7.2.1. SURVEY SOCKET COORDINATES AT 16 MM GAP.

Survey socket designation	Coordinates [mm] ( $\pm 0.05$ mm) ( $\pm 0.2$ mm)					
	X		Y		Z	
	Theoretical	Measured	Theoretical	Measured	Theoretical	Measured
A	200	200.33	335	335.35	1205	1205.0
B	-200	-199.75	335	335.48	1205	1206.0
C	200	200.25	335	335.25	-1205	-1205.0
D	-200	-199.85	335	335.32	-1205	-1203.8
E	200	200.58	-265	-265.64	1205	1205.0
F	-200	-199.47	-265	-265.63	1205	1206.4
G	200	200.33	-265	-265.66	-1205	-1205.0
H	-200	-199.75	-265	265.74	-1205	-1203.5
I	-960	-960.46	680	683.68	990	
J	-960	-959.47	-380.3	-376.40	990	
K	-960	-958.86	680	683.79	-990	
L	-960	-959.42	-380.3	-377.56	-990	

All measures to center of socket hole.

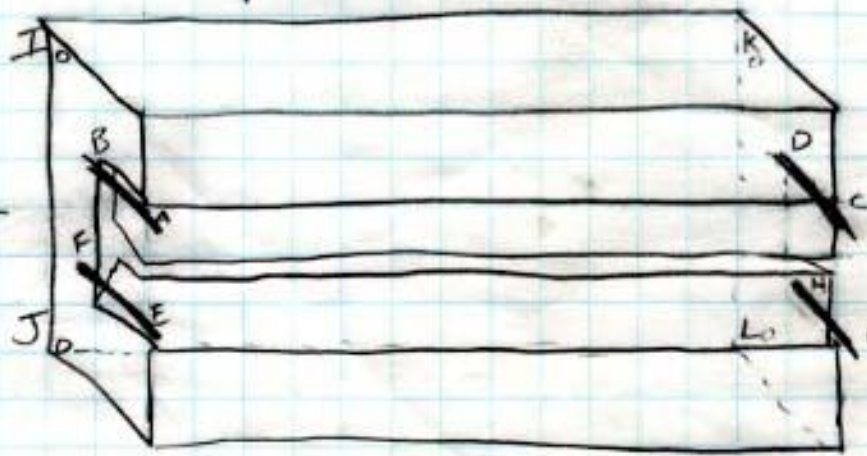


93-0902-1

P @ spot face.  
Add 1.000" to all values for TBS

BL 4 W: 951er

	X			Y			Z	
	mm	in		mm	in		mm	in
A	200.33	7.887	335.35	13.203	1205.0	47.441		
B	-199.75	-7.864	335.48	14.203	1206.0	47.480		
C	200.25	7.884	335.25	13.208	1206.0	47.480		
D	-199.85	-7.868	335.32	14.208	1205.0	-47.441		
E	200.58	7.897	-265.64	13.199	-1205.0	-47.441		
F	-199.47	-7.853	-265.63	14.199	-1203.8	-47.394		
G	200.33	7.887	-265.66	13.202	-1205.0	-47.441		
H	-199.75	-7.864	-265.74	14.202	-1203.5	-47.382		
I	-960.46	-37.813	683.68	-10.458	1205.0	47.441		
J	-959.47	-37.774	-376.40	-9.458	1206.4	47.496		
K	-958.86	-37.750	683.79	-10.458	-1205.0	-47.441		
L	-959.42	-37.772	-377.56	-9.459	-1203.5	-47.382		
				26.917	973.2	38.315		
				27.917	973.2	38.315		
				-14.819	-973.2	-38.315		
				-13.819	-973.5	-38.327		
				26.921	-973.5	-38.327		
				27.921	-973.5	-38.327		
				-14.865	-973.5	-38.327		
				-13.865				



20  
5/20/02

Q)

	<u>G</u>	<u>E</u>	<u>J</u>
VAL	-9.459	-9.458	-13.819
READ	8.452	8.453	12.813
SIT	-1.007	-1.005	-1.006
FT	1	1	1
HI	-0.007 <span style="border: 1px solid black; padding: 2px;">-0.001</span>	-0.005 <span style="border: 1px solid black; padding: 2px;">+0.001</span>	-0.006 ✓

HI = -0.006 ✓

	<u>F</u>	<u>H</u>
HI	-0.006	-0.006
VAL	-9.458	-9.462
~SIT	9.452	9.456
FT	1	1
S/R	8.452	8.456
FND	8.451 <span style="border: 1px solid black; padding: 2px;">+0.001</span>	8.452 <span style="border: 1px solid black; padding: 2px;">+0.004</span> ✓

HI -0.006  
 Blade 25.713  
 @ blade 25.719 ✓

2d  
 5/20/02

HI = 0.000

Pole tips +/- 8mm = +/- 0.315"

	<u>19</u>	<u>15</u>	<u>10</u>	<u>5</u>	<u>1</u>
Top	.330	.314	.315	.309	.324
Bottom	<u>-.318</u>	<u>-.304</u>	<u>-.300</u>	<u>-.313</u>	<u>-.329</u>
Gap	.648 ✓	.618 ✓	.615 ✓	.622 ✓	.653 ✓

Reference Blade

Gun 2

@ 44.354

25.719

HI = 18.635 ✓

<u>J</u>	
READ	31.462
VAL	<u>-13.819</u>
SIT	17.643
FT	<u>1</u>
HI	18.643 ✓

<u>A</u>	<u>B</u>	<u>J</u>	<u>L</u>
18.643	18.643	18.635	18.643
<u>14.203</u>	<u>14.208</u>	<u>-13.819</u>	<u>-13.865</u>
4.440	4.435	32.454	32.508
<u>1</u>	<u>1</u>	<u>1</u>	<u>1</u>
S/R 3.440 ✓	S/R 3.435 ✓	S/R 31.454	S/R 31.508 ✓
FND 3.451 <span style="border: 1px solid black; padding: 2px;">-011</span> ✓	3.452 <span style="border: 1px solid black; padding: 2px;">-017</span> ✓	31.462	31.512 <span style="border: 1px solid black; padding: 2px;">-004</span> ✓

<u>J</u>	<u>C</u>	<u>D</u>	<u>L</u>
READ 31.598	HI 18.779	18.779	18.779
VAL <u>-13.819</u>	VAL 14.199	<u>14.202</u>	<u>-13.865</u>
SIT 17.779	SIT 4.580	4.577 ✓	32.644 ✓
FT <u>1</u>	FT <u>1</u>	<u>1</u>	<u>1</u>
HI 18.779 ✓	S/R 3.580 ✓	3.577	31.644
	FND 3.585 <span style="border: 1px solid black; padding: 2px;">-005</span> ✓	3.586 <span style="border: 1px solid black; padding: 2px;">-009</span> ✓	31.648 <span style="border: 1px solid black; padding: 2px;">-004</span> ✓

28  
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<u>C</u>		<u>K</u>		<u>I</u>	
READ	14.499	HI	29.693		29.693
VAL	14.199	VAL	27.921		27.917
S/I	28.698	S/T	1.772		1.796
FT	1	FT	1		1
S/T	29.698	S/R	.772		.776 ✓
FND	(-0.005)	FND	.778		.791
HI	29.693 ✓		<u>-0.006</u> ✓		<u>-0.015</u> ✓

relative to J being 0

28  
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(X) FAR L	-37.772						
NEAR J	-37.774						
1st F	4.000 +1			2.70			
1st N	7.152 +1			2.760		.92	
2nd F	16.000 +1						
2nd N	14.159 +1						
SIR F	12.580 -1	11.580	11.587	11.571			11.597 +1
SIR N	12.598 -1	11.582	11.592	11.569	11.578		11.595 +1
LOS	50.352						- 50.369 LOS

	<u>K</u>	<u>I</u>	<u>A</u>	<u>B</u>	<u>C</u>
LOS	50.369	50.369	50.369	50.369	50.369
VAL	-37.750	-37.813	7.887	-7.864	7.884
SIT	12.619	12.556	58.256	42.505	58.253
FT	1	1	40.250	40.250	40.250
SIR	11.619 ✓	11.556	18.006 ✓	2.255 ✓	18.003
FND	11.426	11.586	17.974	2.222	17.993
	<u>+ .007 ✓</u>	<u>+ .030 ✓</u>	<u>- .032 ✓</u>	<u>- 033 ✓</u>	<u>- 010</u>

<u>D</u>	<u>E</u>	<u>F</u>	<u>G</u>	<u>H</u>
50.369	50.369	50.369	50.369	50.369
-7.868	7.897	-7.853	7.887	-7.864
42.501	58.268	42.516	58.256	42.505
40.250	40.250	40.250	40.250	40.250
2.251 ✓	18.016 ✓	2.266 ✓	18.006 ✓	2.255 ✓
2.242	17.986	2.232	18.000	2.254
<u>- .009 ✓</u>	<u>- 030 ✓</u>	<u>- 034 ✓</u>	<u>- 006 ✓</u>	<u>- 001 ✓</u>

- C) 7.884
- A) 7.887
- 8.000 +1
- 5.000 +1
- 1.200 +1
- 1.586 +1
- 2.981 -1
- 2.978 -1
- 10.865 ✓

UPPER BLUE MAG. SUPPORT

u/s) 10.865 LOS	o/s) 4.550 3/R ✓
5.315	4.537
<u>5.550</u>	<u>+ 013 ✓</u>
1	
<u>4.550 3/R ✓</u>	
4.540	
<u>+ 010 ✓</u>	

*2B 5/20/20*

SIDE OF MAG.

18 BOT	9.077 +01
TOP	9.097 -00
1 BOT	9.107 -01
1 TOP	9.089 +00

LOWER

4.521	4.514
<u>+ 029 ✓</u>	<u>+ .036 ✓</u>

10.865  
1.772 1/2 MAG  
9.093 3/R

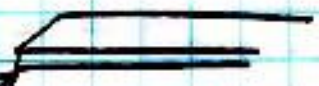
(Y)

Prole

$$HI = -0.006$$

Bottom  
Edge

$$-0.050''$$



SSRL  
Wiggler  $\frac{1}{2}$  H Checked: 8-1-03 JM

7/29/03  
JMc, FG

Wiggler

Y)

J

L

Values

-13.819

-13.869

-13.865

18.865

18.907

.004  
-13.869

.008 mils pitch

3.473

X) (J) Far V. = -37.774  
(L) Near V. = -37.772

K

1st F. = 1 + 1 = 2.000

1st N. = 2.437 + 1 = 3.437

37.750

.007

37.743 cor. val

2nd F. = 3 + 1 = 4.000

2nd N. = 3.264 + 1 = 4.264

42.221

37.743

S/R F. = 4.447 - 1 = 3.447

S/R N. = 4.449 - 1 = 3.449

4.478

1

Los = 42.221

S/R 3.478

3.473

checked  
8-1-03 Jm

SSRL  
Wiggler

B 4  
Chamber

7/29/03  
JMc, FG

Y) Wiggler TBL

$$\begin{array}{r}
 19.149 \\
 \underline{1} \\
 20.149 \\
 \underline{13.869} \\
 HI = 6.280
 \end{array}$$

Chamber

	<u>8</u>	<u>7</u>
	6.280	6.280
	<u>2.967</u>	<u>1.072</u>
	3.313	5.208
	<u>1.25</u>	<u>1.250</u>
SR	2.063	SR 3.958
	2.281	3.861
	2.318	3.960
	<u>2.066</u> [-3]	3.970 -12
	4	<u>3.958</u> [8]
	<u>6.280</u>	
	<u>2.985</u>	
	3.295	
	<u>1.25</u>	
SR	2.045	

Wiggler TBJ

$$\begin{array}{r}
 20.627 \\
 \underline{1} \\
 21.627 \\
 \underline{13.819} \\
 HI = 7.808
 \end{array}$$

Chamber

	<u>3</u>	<u>4</u>	<u>8</u>
	7.908	7.808	7.908
	<u>1.086</u>	<u>2.995</u>	<u>2.967</u>
	6.722	4.823	4.841
	<u>1.250</u>	<u>1.290</u>	<u>1.25</u>
SR	5.472	SR 3.573	SR 3.591
	5.353	3.569 +4	
	5.476	3.573 0	
	5.455	3.575 -2	
	5.465 +7		
	5.419 +3		

SSKL  
# 4 Wiggler Chamber

7/29/03

Checked.  
8-1-03  
JM

X)

$$\begin{array}{r}
 \underline{63} \\
 42.221 \\
 \underline{6.481} \\
 35.740 \\
 \underline{1} \\
 \text{S/R } 34.740 \\
 \underline{1} \\
 34.734 \quad -6
 \end{array}$$

$$\begin{array}{r}
 \underline{7} \\
 42.221 \\
 \underline{6.494} \\
 35.727 \\
 \underline{1} \\
 \text{S/R } 34.727 \\
 \underline{1} \\
 34.728 \quad +1
 \end{array}$$

Z)

$$\begin{array}{r}
 \text{Wiggler} \\
 \underline{F} \\
 25.988 \\
 \underline{1} \\
 26.988 \\
 47.441 \\
 \underline{1} \\
 \text{LOS} = 74.429
 \end{array}$$

$$\begin{array}{r}
 \text{Chamber} \\
 \underline{4} \\
 74.458 \\
 45.475 \\
 \underline{1} \\
 \text{S/R } 27.983 \\
 \underline{1} \\
 27.988 \quad +5
 \end{array}$$

$$\begin{array}{r}
 \underline{F} \\
 25.991 \\
 \underline{1} \\
 26.991 \\
 47.496 \\
 \underline{1} \\
 74.487
 \end{array}$$

LOS = +74.4958

# Final Position of <sup>4</sup>Wiggler Chamber

8-1-03  
JMc, FG.  
Checked.  
8-1-03  
Jm

(X)

LOS = 42.221

2

3

6

7

$$\begin{array}{r}
 42.221 \\
 \underline{6.477} \\
 35.744 \\
 \underline{1} \\
 \text{S/R } 34.744 \\
 \text{FND } 34.737 \quad \boxed{-7}
 \end{array}$$

$$\begin{array}{r}
 \text{S/R } 34.740 \\
 \text{FND } 34.733 \\
 \boxed{-7}
 \end{array}$$

$$\begin{array}{r}
 42.221 \\
 \underline{6.489} \\
 35.732 \\
 \underline{1} \\
 \text{S/R } 34.732 \\
 \text{FND } 34.730 \quad \boxed{-2}
 \end{array}$$

$$\begin{array}{r}
 \text{S/R } 34.727 \\
 \text{FND } 34.726 \\
 \boxed{-1}
 \end{array}$$

4

(Y)

$$\begin{array}{r}
 17.151 \\
 \underline{1} \\
 20.151 \\
 \underline{13.869} \\
 \text{HI} = 6.282
 \end{array}$$

7

8

4

$$\begin{array}{r}
 \text{S/R } 3.960 \\
 \text{FND } 3.950 \\
 \boxed{+10}
 \end{array}$$

$$\begin{array}{r}
 \text{S/R } 2.065 \\
 \text{FND } 2.061 \\
 \boxed{+4}
 \end{array}$$

$$\begin{array}{r}
 \text{S/R } 2.047 \\
 \text{FND } 2.054 \\
 \boxed{+7}
 \end{array}$$

4

$$\begin{array}{r}
 2.985 \\
 \underline{1.067} \\
 2.992 \\
 \underline{2.070} \\
 1.250 \\
 \underline{3.720} \\
 2.992 \\
 \text{HI} = 6.312
 \end{array}$$

3

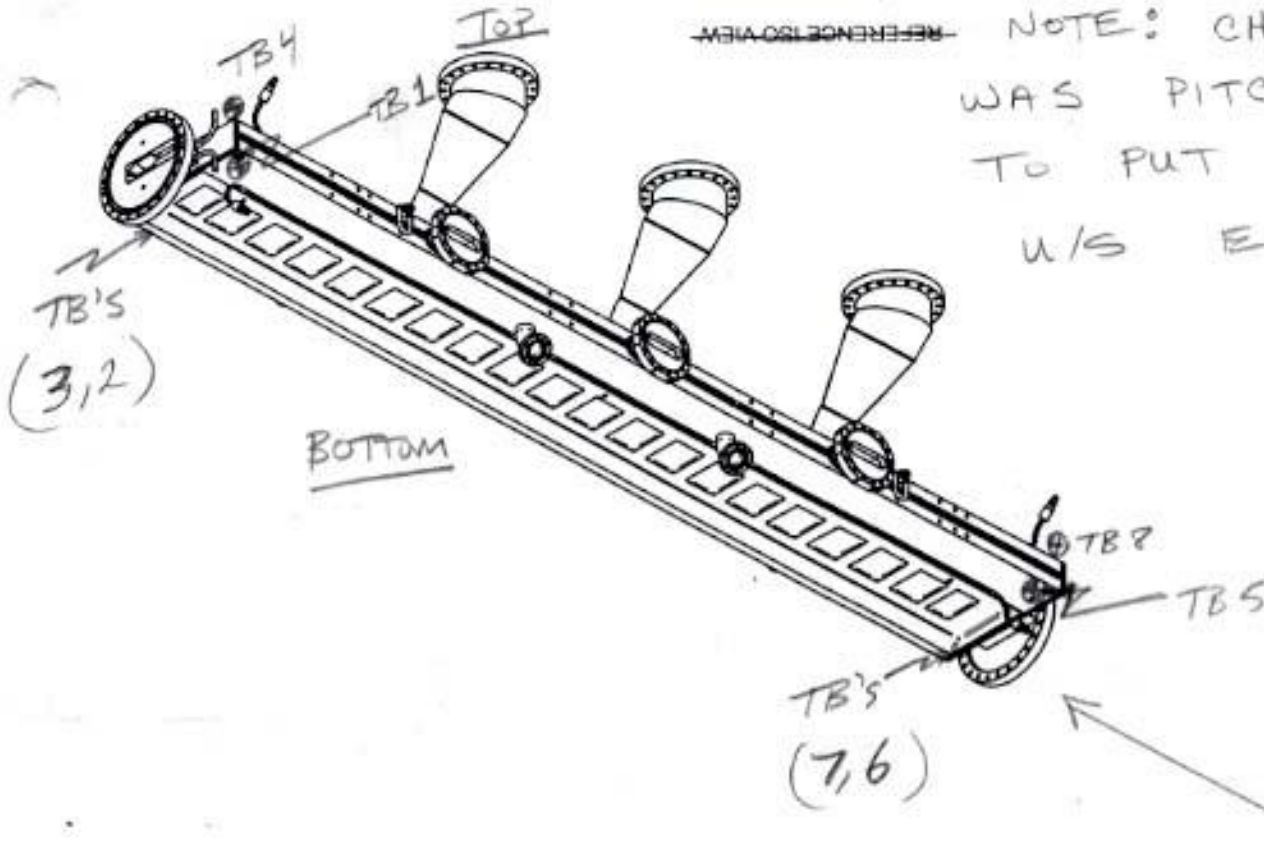
$$\begin{array}{r}
 6.312 \\
 \underline{1.086} \\
 5.226 \\
 \underline{1.250} \\
 \text{S/R } 3.976 \\
 \text{FND } 3.968 \quad \boxed{+8}
 \end{array}$$

Wiggler 5

$$\begin{array}{r}
 6.312 \\
 \underline{13.819} \\
 20.131 \\
 \underline{1} \\
 \text{S/R } 19.131 \\
 \text{FND } 19.131 \quad \phi
 \end{array}$$

# 4 CHAMBER

SC13EDZ



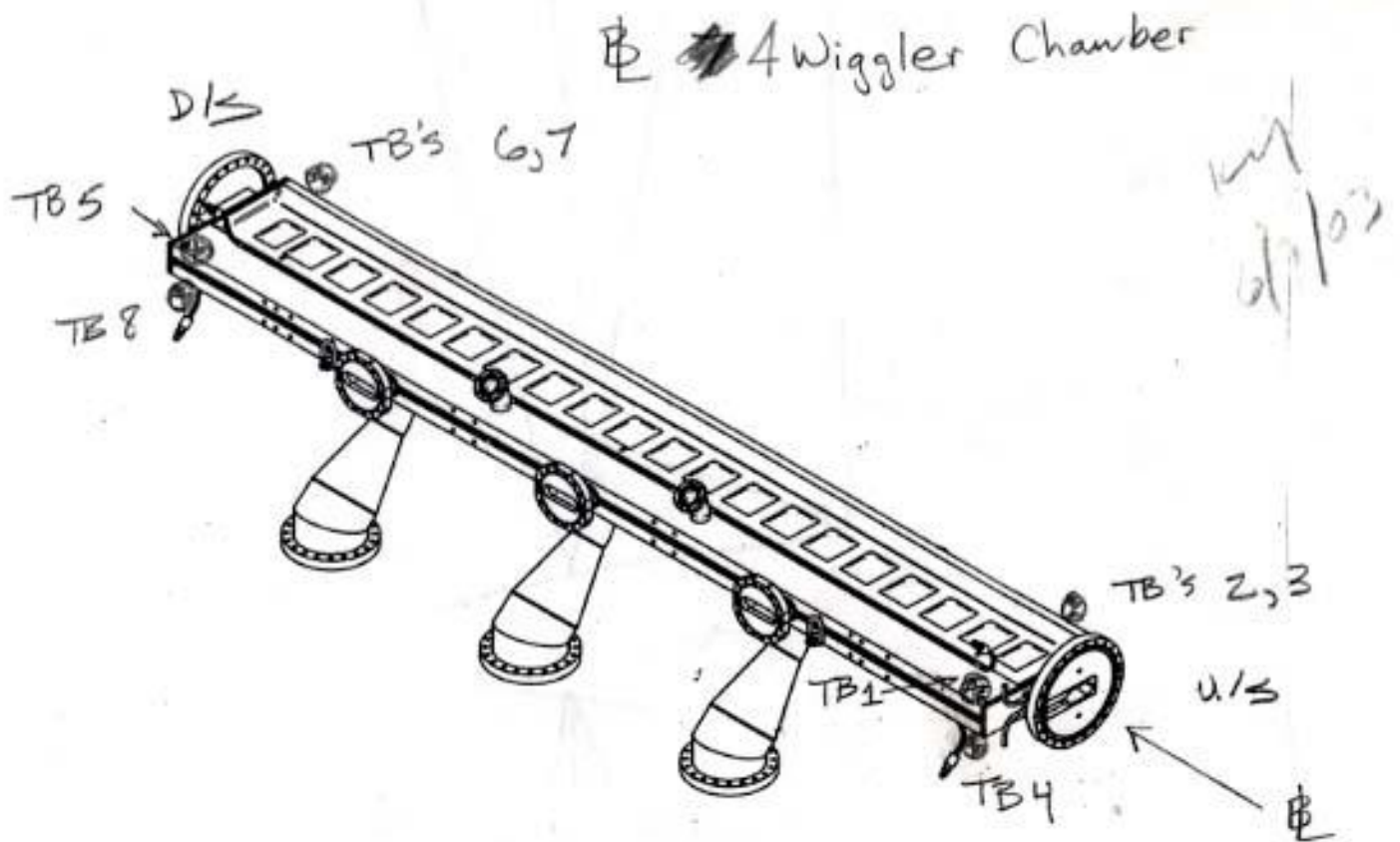
~~REFERENCE VIEW~~

NOTE: CHAMBER WAS PITCHED 180° TO PUT MASK ON U/S END.

## CORRECTED VALUES

TB	Z	X	Y
1	+ 45.485	+7.631	-2.970
2	+ 45.475	-6.477	-1.041
3	+ 45.450	-6.481	+1.086
4	+ 45.475	+7.620	+2.985
5	- 45.465	+7.613	-2.983
6	- 45.485	-6.489	-1.048
7	- 45.485	-6.494	+1.072
8	- 45.465	+7.621	+2.967

	Z	X	Y
1	-45.485	7.631	2.970
2	-45.475	-6.477	1.041
3	-45.450	-6.481	-1.086
4	-45.475	7.620	-2.985
5	45.465	7.613	2.983
6	45.485	-6.489	1.048
7	45.485	-6.494	-1.072
8	45.465	7.621	-2.967



# B 4 Chamber

## PF-444-350-10A

R. Surbaugh 1/4  
H. Imfeld

(V)

Remove Roll from internal chamber.

Set Pitch from W/S & D/S Flanges

$\phi = 9.974$

$\phi = 8.732$

W/S Fl

D/S Fl

READ 4.054  
 VAL 4.987  
 HI 9.041 ✓

4.666  
 4.366  
 9.032 ✓

HI = 9.036 ✓

	1	2	3	5	6	7
HI	9.036	9.036	9.036	9.036	9.036	9.036
READ	5.066	6.995	9.122	5.053	6.988	9.108
S/T	3.970 ✓	2.041 ✓	-.086 ✓	3.983 ✓	2.048 ✓	-.072 ✓
FT	1	1	1	1	1	1
VAL	2.970 ✓	1.041 ✓	<del>.014</del> -1.086 ✓	2.983 ✓	1.048 ✓	<del>.028</del> -1.072 ✓

MIC TB to TB 5 → 8 → (6.450 - .500) = 5.950 - 2.983 = 2.967 ✓

5.950  
 2.983  
 -2.967 ✓

1 → 4 → (6.455 - .500) = 5.955 - 2.970 = 2.985 ✓

Top Spd face 1 - upstream

READ	VAL
1) 8.735	11) .321
2) 8.731	12) .337
3) 8.725	13) .337
4) 8.722	14) .337
5) 8.716	15) .334
6) 8.711	16) .334
7) 8.711	17) .334
8) 8.704	18) .334
9) 8.704	19) .327
10) 8.701	20) .324

10/1  
6/26/03



BOTTOM SPOT FACE (No. 2.604)

OLD CUR → 28.075  
NEW CUR → 16.685  
- 11.390 ✓

OLD HI + 9.036  
NEW HI = -2.354 ✓

1) -2.354 -2.045 - .309	2) -2.354 -2.043 - .311	3) -2.354 -2.044 - .310	4) -2.354 -2.045 - .309
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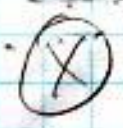
5) -2.354 -2.045 - .309 ✓	6) -2.354 -2.048 - .306 ✓	7) -2.354 -2.048 - .306 ✓	8) -2.354 -2.048 - .306 ✓	9) -2.354 -2.048 - .306 ✓	10) -2.356 -2.047 - .309 ✓
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11) -2.354 -2.055 - .299 ✓	12) -2.354 -2.055 - .299 ✓	13) -2.354 -2.052 - .302 ✓	14) -2.354 -2.054 - .300 ✓	15) -2.354 -2.054 - .300 ✓	16) -2.354 -2.054 - .300 ✓
----------------------------------	----------------------------------	----------------------------------	----------------------------------	----------------------------------	----------------------------------

17) -2.354 -2.055 - .299 ✓	18) -2.354 -2.054 - .300 ✓	19) -2.354 -2.056 - .298 ✓	20) -2.354 -2.056 - .298 ✓
----------------------------------	----------------------------------	----------------------------------	----------------------------------

OLD HI Top + Bottom Pins of U/S + D/S Flanges

	<u>U/S T</u>	<u>U/S B</u>	<u>D/S T</u>	<u>D/S B</u>
HI	9.036	9.036	9.036	9.036
READ	<u>6.526</u>	<u>11.086</u>	<u>6.489</u>	<u>11.056</u>
S/T	2.510 ✓	-2.050 ✓	2.547 ✓	-2.020 ✓
FT	<u>.250</u>	<u>.250</u>	<u>.250</u>	<u>.250</u>
VAL	2.260 ✓	-2.300 ✓	2.297 ✓	-2.270 ✓



FAR 4.987 // U/S Flange  
 NEAR 4.366 // D/S Flange  
 1<sup>st</sup> F 15.000  
 1<sup>st</sup> N 12.093  
 2<sup>nd</sup> F 6.000  
 2<sup>nd</sup> N 10.818  
 SIR F 10.264 //  
 SIR N 10.885 // 10.880 //  
 #1 LOS 15.251 //

FAR -4.987 //  
 NEAR -4.366 //  
 1<sup>st</sup> F -3.000 //  
 1<sup>st</sup> N -2.949 //  
 2<sup>nd</sup> F -4.000 //  
 2<sup>nd</sup> N -4.386 //  
 SIR F -3.578 //  
 SIR N -4.199 //  
 #2 LOS -8.565 //

6/26/03

	1	4	5	8
#1 LOS	15.251	15.251	15.251	15.251
READ	6.620	6.631	6.638	6.630
S/T	8.631	8.620	8.613	8.621
FT	1.000	1.000	1.000	1.000
VAL	7.631	7.620	7.613	7.621

LOS = 8.565 = 2.000 on scale  
 ∴ move gun to 10.565

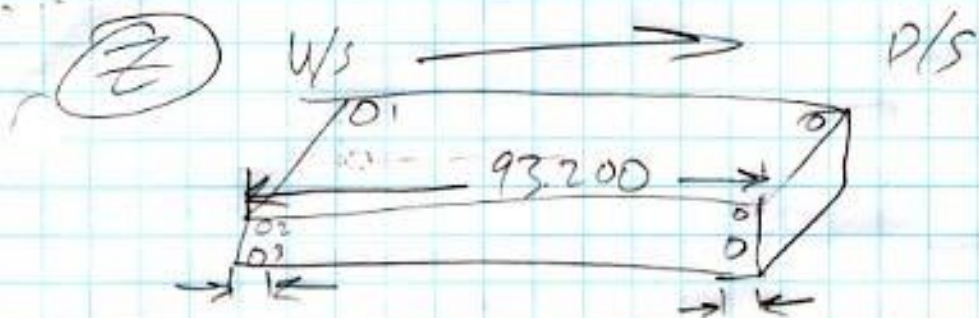
	U/S T	U/S B	D/S T	D/S B
#1	15.251	15.251	15.251	15.251
READ	14.986	14.986	14.986	14.987
S/T	.265	.265	.265	.264
FT	.250	.250	.250	.250
VAL	.015	.015	.015	.014

	2	3	6	7
#2 LOS	-8.565	-8.565	-8.565	-8.565
READ	-1.088	-1.084	-1.076	-1.071
S/T	-7.477	-7.481	-7.489	-7.494
FT	1	1	1	1
VAL	-6.477	-6.481	-6.489	-6.494

MASK U/S

MASK MID

MASK D/S



$$2 \overline{) 46.6} \\ \underline{43.2} \\ 3.4$$

6/26/03

- 1) 1.490 - .375
- 2) 1.500 - .375
- 3) 1.525 - .375
- 4) 1.500 - .375

- 5) 1.510 - .375
- 6) 1.490 - .375
- 7) 1.490 - .375
- 8) 1.510 - .375

<u>1</u>	<u>2</u>	<u>3</u>	<u>4</u>	<u>5</u>	<u>6</u>
-46.600	-46.600	-46.600	-46.600	46.600	46.600
<u>1.490</u>	<u>1.500</u>	<u>1.525</u>	<u>1.500</u>	<u>-1.510</u>	<u>-1.490</u>
-45.110	-45.100	-45.075	-45.100	45.090	45.110
<u>-.375</u>	<u>-.375</u>	<u>-.375</u>	<u>-.375</u>	<u>.375</u>	<u>.375</u>
45.485	45.475	45.450	45.475	45.465	45.485

<u>7</u>	<u>8</u>
46.600	46.600
<u>-1.490</u>	<u>-1.510</u>
45.110	45.090
<u>.375</u>	<u>.375</u>
45.485	45.465