

Beam Line 14-1 Summary

<u>Mask 2</u>	<u>Mask 3</u>	<u>Vert. Slits</u>	<u>Graphite Filter</u>
X= -.001	X= -.014	Top X= .020 Y= -.019	X= .003
Y= -.003	Y= .000	Bottom X= -.027 Y= -.006	Y= .000
Z= 630.2	Z= -.012	Z= -.012	Z= -.012
Roll= 0	Roll= 0		Roll = +.2 mr
			Yaw= .000 mr

<u>Slit Package Tanks</u>	<u>U/S Be Window</u>	<u>D/S Be Window</u>	<u>Mono</u>
Y = .001	Y's (+)= .004, (+)= .007	X = .006	X = .003
X = .003		Y = -.002	Y = -.002
Z = -.012		Roll = .000	Z = .005
			Roll= .000
			Yaw = .23 mr
			Pitch = 0.04 mr

<u>M1Mirror Tank</u>	<u>M1 Mirror Plate</u>	<u>Hutch Stopper</u>
X = .000	X = .004	X= .054
Y = -.001	Y = Moveable ?	Y= .000
	Z = .013	
	Roll = .36 mr	
	Yaw = .04 mr	
	Pitch= .04 mr	

Collimator

X= -.005
 Y= -.001
 Roll = 1 mr
 Yaw = 2.8 mr
 Pitch = .5 mr

Y

SSRL

2-19-09
M.R., L.G.

BL14F19

574.74004 EL
- 575.7911 BL
-1.05106 M
-41.380" ✓

17.271
40.750
58.021 ✓
41.380
16.641 ✓

HRL5105

574.72709
- 575.7911
-1.06401 M
-41.890" ✓

17.779
40.750
58.529 ✓
41.890
16.639 ✓

$\bar{M} = 16.640"$ ✓

SLIT TANK

1) 16.640
- 2.208
18.848 ✓
17.848 s/r ✓
- .156
17.692 s/r
17.694
+0.001

G.F. TANK

1) 16.640
- 2.333
18.973 ✓
17.973 s/r
17.978
+0.002

3) 16.640
- 2.252
18.892 ✓
17.892 s/r ✓
17.891
+0.001

PHOT MASK 2 SA 451-091-47

16.640
2.250 & APER FROM FLAT
14.390 ✓
- 1.512 offset (slope)
15.902 s/r ✓

(+) 15.905 (-) 15.905
-0.003 -0.003

SSRL
BL 14-1

2-20-09
M.R., L.C.

MASK 3 w/s Vent SLIT TANK

① +16.640 HI

(+) 16.640 (-) 16.640
2.258 2.257 FLAT

✓ 14.382

✓ 14.383

-2.107

-2.107

OFFSET FROM SPEAR

✓ 16.489 5/12

✓ 16.490 5/12

16.489

16.489

✓ \ominus

✓ +001

② +25.591 LOS

+ SIDE TOP

25.591

2.249 FLAT

✓ 23.342

-5.533 OFFSET FROM 14-2

✓ 28.875

28.889

✓ - .014

SSRL
 BL 14-1
 VERT. SLIT. PACKAGE
 & MASK 2

2-20-09
 M.R., L.G

(X) .65M = +25.59/LOS

MASK 2

25.591
 - 5.039 OFFSET (629.921 x .008)

30.630
 2.309R (4.618φ)

28.3215/R

28.322

-001

VERT. SLIT TANK

1) 25.591
 - 2.026
 27.617
 13.000 SURF
 14.6175/R
 14.620
 -003

G.F. TANK

2) 25.591^(T)
 - 2.092
 27.683
 13. —
 14.6835/R
 14.685
 -002

G.F.

5) 25.591
 - 3.586
 29.177
 13. —
 16.1775/2
 16.157
 +020

SLITS

6) 25.591^(B)
 - 3.584
 29.175
 13. —
 16.1755/R
 16.202
 -027

VST

3) 25.591
 - 1.074

26.665

13. —

13.6655/R

13.655

1) 25.591
 - 1.886
 27.477
 13. —
 14.4775/R
 14.467
 +010

A) 25.591
 - 5.997
 31.588
 13. —
 18.5885/R
 18.584
 +004

D) 25.591
 - 5.953
 31.544
 13. —
 18.5445/R
 18.542
 +002

SSRL
BL 4-1

2-20-09
M.R., L.G.

① 16.640 HI

VERT SLITS

$$5) \begin{array}{r} 16.640 \\ - 9.567 \\ \hline \end{array}$$

$$\begin{array}{r} \sqrt{7.073} \\ 1. \text{---} \\ \hline \end{array}$$

C.210 $\begin{array}{r} \sqrt{6.073 \text{ S/R}} \\ 6.092 \end{array}$

$$\boxed{-019}$$

$$6) \begin{array}{r} 16.640 \\ - 13.900 \\ \hline \end{array}$$

$$\begin{array}{r} \sqrt{30.540} \\ 23.496 \\ \hline \end{array}$$

$$\begin{array}{r} \sqrt{7.044} \\ 1250 \frac{1}{2} \text{ T/B} \\ \hline \end{array}$$

$$\begin{array}{r} \sqrt{6.794 \text{ S/R}} \\ 6.800 \end{array}$$

$$\boxed{-006}$$

TANK

$$2) \begin{array}{r} 16.640 \\ - 2.377 \\ \hline \end{array}$$

$$\begin{array}{r} \sqrt{19.017} \\ 1. \text{---} \\ \hline \end{array}$$

$$\begin{array}{r} \sqrt{18.017 \text{ S/R}} \\ 18.627 \end{array}$$

$$\boxed{-010}$$

$$3) 16.640$$

23.496

SSRL

BL 14-1

2-20-09
M.R., L.G.

(Y) +16.640 HI

FIX GRAPHITE FILTER

A) 16.640 4.029 ----- 12.611 1. ——— ----- 11.611 S/R 11.611 ----- [\emptyset]	B) 16.640 4.071 ----- 12.569 1. ——— ----- 11.569 S/R 11.569 ----- [\emptyset]	C) 16.640 4.048 ----- 12.592 1. ——— ----- 11.592 S/R 11.590 ----- [+002]	D) 16.640 4.098 ----- 12.542 1. ——— ----- 11.542 S/R 11.542 ----- [\emptyset]
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(Z) 18M = 708.661"

G.F. TANK

708.661
(-).058

708.603 LOS

1) 708.603
711.118

2.515
1. ———

1.515 S/R
1.527

[-012]

U.S. TANK

1) 694.087 VAL.
63.875

630.212
629.921 S/B

[+.291]

SSRL
BL 14-1
MANO

3-2-09

J.M., L.G.

Y

HRLS105

7.344
57.750
65.094
- 41.890 EL.
23.204

BL14F19

6.835
57.750
64.585
- 41.380
23.205

o/s Ba
- 2.367 Y
719.000 Z
u/s Ba
- 2.341 Y
716.278 Z

$\bar{M} = 23.205 \pm I$

PINS

u/s) 23.205
- 2.496

25.701
.126

25.575

(+) .167

25.468 3/4

25.468

0

2.162

o/s) 23.205
- 2.496 & SPINDLE

25.701

.126 R DOWEL PIN

25.575

(-) .167 Pitch = 9.6 MR

25.682 3/4

25.681

+001

Be WINDOWS

2.108

Pitch
10.4 MR

o/s) 23.205

- 2.367

25.572

2.162

23.410 5/8

+) 23.412

-002

-) 23.412

-002

u/s) 23.205

- 2.341 &

25.546

2.108 TO TOP

23.438

.138 7/8 &

23.300 3/4

+) 23.296

+004

-) 23.293

+007

(Y)

+23.211 HI

SSRL
BL14-1
MONO

2-27-09
J.M., BR, L. G

4620 ϕ U/S

FLANGES
U/S

PINS

22.288 $\Delta Z = .214$ NY

u/s) 23.211
 .2.496

 25.707
 .126

 25.581
 CA: 1.07

 25.4745/R
 25.475

d/s) 23.211
 -2.496 ϕ SPINDLE

 25.707
 .126 R. PIN

 25.581
 (-).107 Pitch 9.6MR

 25.688 S/R
 25.687

Y =
Z = 719.000

P/S

Y =
Z = 745.482

Pitch:
1.09 MR

-1.

+1

(X)

-27.559" LOS 3-2-09

Roll (MONO FACE PLATE)

TOP) 16.627 BOT) 16.627

3-2-09

(Z) 19.25M = 757.874"

757.874

745.482 P/S FL FACE

12.392

1750 FACE OF FL
LOPER

11.642

6.700 SPUR

4.9425/R

4.937

+0.005

ROLL

TOP

16.627

BOT

16.627 ϕ

YAW

.23 MR

FLANGES

D/S B2

u/s) 27.559
 2.310

 25.249
 -5.752

 19.497
 3.500

 22.9975/R
 23.003

 +.006

d/s) 27.559
 2.310 RAD.

 25.249
 -5.964 YAW

 19.285
 3.500 BUCKLE

 22.785 S/R
 22.785

 +.006

Y

SSRL
BL14-1
MI-MIRROR

2-26-09
B.R., J.M., L.G.

HRLS105
 7.350
 57.750

 65.100
 41.890

 23.210

BL14F19
 6.841
 57.750

 64.591
 41.380

 23.211

$\bar{M} = 23.211 \text{ HI}$

MI-MIRROR TANK

1) 23.211
 -11.842

 35.053
 1. ———

 34.053 S/R
 34.054

 -001

2) 23.211
 -11.824

 35.035
 1. ———

 34.035 S/R
 34.037

 -002

3) 23.211
 -11.875

 35.086
 21.227

 13.859 S/R
 13.858

 +001

Y $\bar{M} = 27.559$
 X $.7M = 27.559'' \text{ WS}$

3) 27.559
 -11.914

 15.645
 1. ———

 14.645 S/R
 14.645

 +0

4) 27.559
 -12.255

 15.304
 1. ———

 14.304 S/R
 14.304

 -0

SSRL
BL 14-1
MI-MIRROR
TILT PLATE

2-26-09
B.R., J.M., L.G.

④

23.211 HI

TILT PLATE

$$\begin{array}{r}
 \text{A) } 23.211 \\
 - 19.452 \\
 \hline
 42.663 \\
 21.227 \\
 \hline
 21.436 \\
 18.000 \\
 \hline
 3.436 \text{ s/r} \\
 3.433 \\
 \hline
 \boxed{+0.003}
 \end{array}$$

$$\begin{array}{r}
 \text{B) } 23.211 \\
 - 19.427 \\
 \hline
 42.638 \\
 21.227 \\
 \hline
 21.411 \\
 18.000 \\
 \hline
 3.411 \text{ s/r} \\
 3.415 \\
 \hline
 \boxed{+0.004}
 \end{array}$$

$$\begin{array}{r}
 \text{C) } 23.211 \\
 - 19.464 \text{ VAL} \\
 \hline
 42.675 \\
 21.227 \text{ FT} \\
 \hline
 21.448 \\
 18.000 \text{ SPLICE} \\
 \hline
 3.448 \text{ s/r} \\
 3.448 \\
 \hline
 \boxed{\emptyset}
 \end{array}$$

3.000

3.300

80

3.410

Roll 71
1.36 MRU

⑤ - 27.559"

$$\begin{array}{r}
 \text{C) } 27.559 \\
 10.354 \\
 \hline
 17.203 \\
 12.528 \\
 \hline
 4.675 \text{ s/r} \\
 4.678 \\
 \hline
 \boxed{+0.003}
 \end{array}$$

$$\begin{array}{r}
 \text{D) } 27.559 \\
 10.443 \text{ VAL} \\
 \hline
 17.116 \\
 17.000 \text{ FT} \\
 \hline
 16.116 \text{ s/r} \\
 16.120 \\
 \hline
 \boxed{+0.004}
 \end{array}$$

678 + 3
120 + 4

2-27-09
BR, JM, LG

SSRL
BL14-1
MIRROR
LIMITS

(X)

-27.559605

(+) LIMIT

c) $\frac{4.678}{4.675 \text{ s/r}}$

d) $\frac{16.163}{16.116}$
 $.047 - .004 = .043 \Delta$ (START)
✓

(-) LIMIT

c)

d) $\frac{16.082}{16.120 \text{ START}}$
 $[-038]$ ✓

✓ BR
2/27/09

FINAL ϕ YAW @ -8 MRZ

c) $\frac{27.559}{10.356}$
 17.203
 12.528 off H
 $\frac{4.675 \text{ s/r}}{4.678}$
 $[+003]$ ✓

d) $\frac{27.559}{10.443}$
 17.116
 $1.$
 $\frac{16.116 \text{ s/r}}{16.120}$
 $[+004]$ ✓

SSRL
BL14-1
M1 MIRROR

2-27-09
JM, BR, LG

Setting of CHECKING LIMITS

①

Pitch +.5MR

- z
A) 11.232
B) 14.004

$$\frac{25.236}{11.232} \times .5MR = .10126 \Delta Y$$

- A) -.006 B) +.006

✓ BR
2/27/09

$$25.236 \times 11.1MR = .280 \Delta Y$$

- A) 3.436 s/r ϕ B) 3.411 s/r ϕ
 $\frac{+ .140}{3.296 \text{ s/r } \checkmark}$ $\frac{+ .140}{3.551 \text{ s/r } \checkmark}$ Pitch DN 11.1MR

$$\text{FINAL} = 9.6MR \times 25.236 = .242 \Delta Y$$

- A) 3.436 B) 3.411
 $\frac{+ .121}{3.315 \text{ s/r } \checkmark}$ $\frac{+ .121}{3.532 \text{ s/r } \checkmark}$
A B
 LIMITS

- A) 3.000 READ B) 3.118 READ
 $\frac{3.436 \text{ s/r}}{+ .436 \checkmark}$ $\frac{3.411 \text{ s/r}}{+ .293 \checkmark}$

- A) 3.776
 3.436 s/r
+ .334 ✓

- B) 3.905
 3.411 s/r
 $\frac{- .494}{\checkmark}$

SSRL

BL 14-1

3-2-09

HUTCH STOPPER

Y +23.205 HT

1) 23.205
 .224
 22.979
 1.
 21.979 s/r
 21.980
 -001

2) 23.205
 .234
 22.971
 1.
 21.971 s/r
 21.971
 -01

3) 23.205
 .781
 22.424
 1.
 21.424 s/r
 21.424
 -06

4) 23.205
 .781
 22.424
 1.
 21.424 s/r

X +25.591 WS

1) 25.591
 614.285
 29.876
 1.
 28.876 s/r
 25.
 3.876 s/r
 3.880
 -004

2) 25.591
 414.562
 30.153
 1.
 29.153
 25. SLICE
 4.153 s/r
 4.158
 -005

3-12-09
 3.7855
 +091

3-12-09
 4.170
 -017

Z

815.901 D/S W1
 820.792 U/S #5
 4.891
 .875 FL. COVER
 4.014
 750 FL COVER
 3.264

7/8 3/4

3-12-09
 USED STOPPER TO
 SET D/S COLLIMATOR
 "X"

SSRL
BL14-1
COLLIMATOR

3-12-09
J.M., M.R., L.G.

(Y)

BL14F19
6.270
57.750
64.020
-41.380
22.640

HRLS105
6.778
57.750
64.528
-41.890
22.638

u/s .900
p/s .892

$\bar{M} = 22.639 \text{ HI}$

COLLIMATOR

y/s
u/s) (+) .875 (-)
p/s) (+) .890 (-) .882

u/s
(+) 22.639
-2.588
25.227
+ .438 $\frac{1}{2}$ coll.
24.789 $\frac{1}{2}$
24.799
- .010

D/S
(+) 22.639 (-) 22.639
-2.588
25.227
+ .445
24.782 $\frac{1}{2}$
24.777
+ .005

(-) 22.639
-2.588
25.227
+ .441
24.786 $\frac{1}{2}$
24.783
+ .003

+5

(X) .65M = 25.591 $\frac{1}{2}$

u/s) 25.591
1.005 $\frac{1}{2}$
24.586
 \leftarrow 6.702 yaw
31.288
20. \leftarrow SPURF
11.288 $\frac{1}{2}$
11.294
- .006

D/S) 25.591
1.005
24.586
 \leftarrow 6.780
31.366
20. \leftarrow
11.366 $\frac{1}{2}$
11.369
- .003

x/s
u/s) 2.010
D/S) 2.010

z/s
u/s 835.799
472. \leftarrow
837.799
yaw -6.702
o/s 849.528
-2. \leftarrow
847.528 $\Delta z = 9.729$
-6.780

SSRL
BL 14-1

3-12-09
JM, MR, LG

(A) +22,639 HI
3" Pipe

4/s
22.639
1.500 R

21.139
-2.588 offset

23.727 s/r
23.710

+1.017

HI
0.5 Hz
23.727 s/r
690
+1.037

(X) +25.591 LOS HI

.75u = +29.528 H2 WS

4/s
+7

25.591
1.500 R

24.091
-6.852 Yaw

30.943
30.958

-0.015

MID
+105

29.528
1.500

28.028
-7.692

35.720
35.798

+0.022

D/S
+213

29.528
1.500

28.028
-8.500

36.528
36.509

+0.019

(Z)

849.528

4/s 856.528

MID 961.528

D/S 1062.528

SSRL
BL14-1

3-12-09
MR, JM, LG

(Y)

BF1429
 574.72718
 575.7911

 -1.06392M
 -41.887"
 9.769
 40.750

 50.519
 -41.887 EL

 8.632

ARLS 110
 574.72994
 575.7911

 -1.06116M
 -41.778"
 9.663
 40.750

 50.413
 -41.778

 8.635

M = 8.634 HI
PIPE
HATCH 2

MID
 8.634
 1.500 R

 7.134
 -2.588

 9.722 S/R
 9.713

 +.009

P/S
 8.634
 1.500

 7.134
 -2.588

 9.722 S/R
 9.720

 +.002

H 2
 SH 3
 9.728

 -006

H 1
 OS H 2
 17.037

PIPE @ FLANGE

9815

 -093