

Transverse to Longitudinal Emittance Exchange

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- Idea proposed by M. Cornacchia (Nov. 2001)
- Analysis taken from similar work by W. Spence and PE (unpublished, ~1990)
- Motivation to reduce transverse emittance and increase longitudinal emittance — faster SASE X-ray FEL lasing and less CSR micro-bunching in compressors

X-ray SASE FEL needs emittance...

$$\gamma \varepsilon_x < \gamma \frac{\lambda_r}{4\pi},$$

and energy spread...

$$\sigma_\delta < \rho \approx \frac{1}{4} \left(\frac{1}{2\pi^2} \frac{I_{pk}}{I_A} \frac{\lambda_u^2}{\beta \varepsilon_N} \left(\frac{K}{\gamma} \right)^2 \right)^{1/3}.$$

At $\lambda_r \approx 1 \text{ \AA}$ and $\gamma \approx 3 \times 10^4 \rightarrow \gamma \varepsilon_x < \mathbf{0.2 \mu m}$

But $\sigma_\delta < 0.09\%$ (for $I_{pk} \approx 4 \text{ kA}$, $\lambda_u \approx 3 \text{ cm}$, $K \approx 4$, $\beta \approx 20$)

This means $\gamma \sigma_z \sigma_\delta = \gamma \varepsilon_z < \mathbf{500 \mu m}$

RF-guns produce $\gamma \varepsilon_x \sim 5 \mu m$ and $\gamma \varepsilon_z \sim 2 \mu m$
(and highly variable)

Can we exchange these in some way,
reducing ε_x while increasing ε_z (maybe also
damping the CSR microbunching) ?

Initial uncoupled 4×4 beam covariance matrix $\boldsymbol{\sigma}_0$ [$\gamma_x = (1 + \alpha_x^2)/\beta_x$, $\gamma_z = (1 + \alpha_z^2)/\beta_z$]...

$$\boldsymbol{\sigma}_0 = \begin{pmatrix} \varepsilon_{x_0} \beta_x & -\varepsilon_{x_0} \alpha_x & 0 & 0 \\ -\varepsilon_{x_0} \alpha_x & \varepsilon_{x_0} \gamma_x & 0 & 0 \\ 0 & 0 & \varepsilon_{z_0} \beta_z & -\varepsilon_{z_0} \alpha_z \\ 0 & 0 & -\varepsilon_{z_0} \alpha_z & \varepsilon_{z_0} \gamma_z \end{pmatrix}$$

$$= \begin{pmatrix} \boldsymbol{\sigma}_x & \mathbf{0} \\ \mathbf{0} & \boldsymbol{\sigma}_z \end{pmatrix}$$

$$\sigma_x = \sqrt{\varepsilon_{x_0} \beta_x}, \quad \sigma_z = \sqrt{\varepsilon_{z_0} \beta_z}$$

$$\text{chirp: } \frac{\langle z\delta \rangle}{\sigma_z^2} = -\frac{\alpha_z}{\beta_z}, \quad (\delta \equiv \Delta E/E_0)$$

$$E\text{-spread: } \sigma_\delta = \sqrt{\varepsilon_z (1 + \alpha_z^2) / \beta_z} = \sqrt{\sigma_{\delta_u}^2 + \sigma_{\delta_c}^2}$$

$$\gamma \varepsilon_z = \gamma \sqrt{\sigma_z^2 \sigma_\delta^2 - \langle z\delta \rangle^2}$$

$$\gamma \varepsilon_z (\alpha_z = 0) = \gamma \sigma_z \sigma_\delta = \sigma_z \frac{\sigma_E}{mc^2}$$

Propagate $\boldsymbol{\sigma}_0$ through 4×4 transfer matrix, \mathbf{R}

$$\boldsymbol{\sigma} = \mathbf{R} \boldsymbol{\sigma}_0 \mathbf{R}^T,$$

which is four 2×2 blocks

$$\mathbf{R} = \begin{bmatrix} \mathbf{A} & \mathbf{B} \\ \mathbf{C} & \mathbf{D} \end{bmatrix},$$

$$\mathbf{A} = \begin{pmatrix} a_{11} & a_{12} \\ a_{21} & a_{22} \end{pmatrix}, \quad \mathbf{B} = \begin{pmatrix} b_{11} & b_{12} \\ b_{21} & b_{22} \end{pmatrix}, \quad \text{etc.}$$

$$\boldsymbol{\sigma} = \begin{pmatrix} \mathbf{A} \boldsymbol{\sigma}_x \mathbf{A}^T + \mathbf{B} \boldsymbol{\sigma}_z \mathbf{B}^T & \mathbf{A} \boldsymbol{\sigma}_x \mathbf{C}^T + \mathbf{B} \boldsymbol{\sigma}_z \mathbf{D}^T \\ \mathbf{C} \boldsymbol{\sigma}_x \mathbf{A}^T + \mathbf{D} \boldsymbol{\sigma}_z \mathbf{B}^T & \mathbf{C} \boldsymbol{\sigma}_x \mathbf{C}^T + \mathbf{D} \boldsymbol{\sigma}_z \mathbf{D}^T \end{pmatrix}$$

$$\varepsilon_x^2 = \left| \mathbf{A} \boldsymbol{\sigma}_x \mathbf{A}^T + \mathbf{B} \boldsymbol{\sigma}_z \mathbf{B}^T \right|$$

$$\varepsilon_z^2 = \left| \mathbf{C} \boldsymbol{\sigma}_x \mathbf{C}^T + \mathbf{D} \boldsymbol{\sigma}_z \mathbf{D}^T \right|$$

Determinant of sum of 2×2 matrices...

$$|\mathbf{X} + \mathbf{Y}| = |\mathbf{X}| + |\mathbf{Y}| + \text{tr} \{ \mathbf{X}^a \mathbf{Y} \},$$

where \mathbf{X}^a is the adjoint of \mathbf{X} ...

$$\mathbf{X}^a = |\mathbf{X}| \mathbf{X}^{-1}, \quad |\mathbf{X}| \neq 0, \quad \text{or}$$

$$\mathbf{X}^a = \mathbf{J}^{-1} \mathbf{X}^T \mathbf{J}$$

and \mathbf{J} is...

$$\mathbf{J} \equiv \begin{pmatrix} 0 & 1 \\ -1 & 0 \end{pmatrix}, \quad \mathbf{J}^2 = -\mathbf{I}.$$

The emittances are...

$$\varepsilon_x^2 = |\mathbf{A}|^2 \varepsilon_{x_0}^2 + |\mathbf{B}|^2 \varepsilon_{z_0}^2 + tr \left\{ \left(\mathbf{A} \boldsymbol{\sigma}_x \mathbf{A}^T \right)^a \mathbf{B} \boldsymbol{\sigma}_z \mathbf{B}^T \right\},$$

$$\varepsilon_z^2 = |\mathbf{C}|^2 \varepsilon_{x_0}^2 + |\mathbf{D}|^2 \varepsilon_{z_0}^2 + tr \left\{ \left(\mathbf{C} \boldsymbol{\sigma}_x \mathbf{C}^T \right)^a \mathbf{D} \boldsymbol{\sigma}_z \mathbf{D}^T \right\}$$

Now use alternate form for $\boldsymbol{\sigma}_{x,z}$...

$$\boldsymbol{\sigma}_x = \varepsilon_{x_0} \mathbf{Q}_x \mathbf{Q}_x^T, \quad \mathbf{Q}_x \equiv \frac{1}{\sqrt{\beta_x}} \begin{pmatrix} \beta_x & 0 \\ -\alpha_x & 1 \end{pmatrix},$$

and also use property of trace...

$$tr \{ XYZ \} = tr \{ YZX \} = tr \{ ZXY \}$$

Emittances are then...

$$\varepsilon_x^2 = |\mathbf{A}|^2 \varepsilon_{x_0}^2 + |\mathbf{B}|^2 \varepsilon_{z_0}^2 + \varepsilon_{x_0} \varepsilon_{z_0} \text{tr} \{ \mathbf{U} \mathbf{U}^T \},$$

$$\varepsilon_z^2 = |\mathbf{C}|^2 \varepsilon_{x_0}^2 + |\mathbf{D}|^2 \varepsilon_{z_0}^2 + \varepsilon_{x_0} \varepsilon_{z_0} \text{tr} \{ \mathbf{V} \mathbf{V}^T \},$$

where

$$\mathbf{U} \equiv \mathbf{Q}_x^{-1} \mathbf{A}^a \mathbf{B} \mathbf{Q}_z,$$

$$\mathbf{V} \equiv \mathbf{Q}_x^{-1} \mathbf{C}^a \mathbf{D} \mathbf{Q}_z.$$

Now use the symplectic condition...

$$\mathbf{R}^T \mathbf{S} \mathbf{R} = \mathbf{R} \mathbf{S} \mathbf{R}^T = \mathbf{S} = \begin{pmatrix} \mathbf{J} & \mathbf{0} \\ \mathbf{0} & \mathbf{J} \end{pmatrix}$$

$$\mathbf{R}^T \mathbf{S} \mathbf{R} = \begin{pmatrix} \mathbf{A}^T \mathbf{J} \mathbf{A} + \mathbf{C}^T \mathbf{J} \mathbf{C} & \mathbf{A}^T \mathbf{J} \mathbf{B} + \mathbf{C}^T \mathbf{J} \mathbf{D} \\ \mathbf{B}^T \mathbf{J} \mathbf{A} + \mathbf{D}^T \mathbf{J} \mathbf{C} & \mathbf{B}^T \mathbf{J} \mathbf{B} + \mathbf{D}^T \mathbf{J} \mathbf{D} \end{pmatrix} =$$

$$\mathbf{R} \mathbf{S} \mathbf{R}^T = \begin{pmatrix} \mathbf{A} \mathbf{J} \mathbf{A}^T + \mathbf{B} \mathbf{J} \mathbf{B}^T & \mathbf{A} \mathbf{J} \mathbf{C}^T + \mathbf{B} \mathbf{J} \mathbf{D}^T \\ \mathbf{C} \mathbf{J} \mathbf{A}^T + \mathbf{D} \mathbf{J} \mathbf{B}^T & \mathbf{C} \mathbf{J} \mathbf{C}^T + \mathbf{D} \mathbf{J} \mathbf{D}^T \end{pmatrix}$$

$$|\mathbf{A}^T \mathbf{J} \mathbf{A} + \mathbf{C}^T \mathbf{J} \mathbf{C}| = |\mathbf{A} \mathbf{J} \mathbf{A}^T + \mathbf{B} \mathbf{J} \mathbf{B}^T| = 1,$$

$$|\mathbf{B}^T \mathbf{J} \mathbf{B} + \mathbf{D}^T \mathbf{J} \mathbf{D}| = |\mathbf{C} \mathbf{J} \mathbf{C}^T + \mathbf{D} \mathbf{J} \mathbf{D}^T| = 1$$

and find the relations between the sub-matrix determinants...

$$|\mathbf{A}| + |\mathbf{C}| = \pm 1, \quad |\mathbf{A}| = |\mathbf{D}|, \quad |\mathbf{B}| = |\mathbf{C}|,$$

and also between \mathbf{U} and \mathbf{V} ...

$$\mathbf{V} \equiv \mathbf{Q}_x^{-1} \mathbf{C}^a \mathbf{D} \mathbf{Q}_z = \mathbf{Q}_x^{-1} (\mathbf{J}^{-1} \mathbf{C}^T \mathbf{J}) \mathbf{D} \mathbf{Q}_z,$$

and using from above...

$$\mathbf{C}^T \mathbf{J} \mathbf{D} = -\mathbf{A}^T \mathbf{J} \mathbf{B},$$

$$\begin{aligned} \mathbf{V} &\equiv -\mathbf{Q}_x^{-1} \mathbf{J}^{-1} (\mathbf{A}^T \mathbf{J} \mathbf{B}) \mathbf{Q}_z \\ &= -\mathbf{Q}_x^{-1} \mathbf{A}^a \mathbf{B} \mathbf{Q}_z = -\mathbf{U} \end{aligned}$$

Therefore,

$$tr\{\mathbf{U}\mathbf{U}^T\} = tr\{\mathbf{V}\mathbf{V}^T\}$$

which is the sum of squares of the normalized coupling matrix, and is positive.

$$tr\{\mathbf{U}\mathbf{U}^T\} = U_{11}^2 + U_{12}^2 + U_{21}^2 + U_{22}^2 \equiv \lambda^2 \geq 0$$

The emittances are...

Transverse RF accelerates and kicks beam...

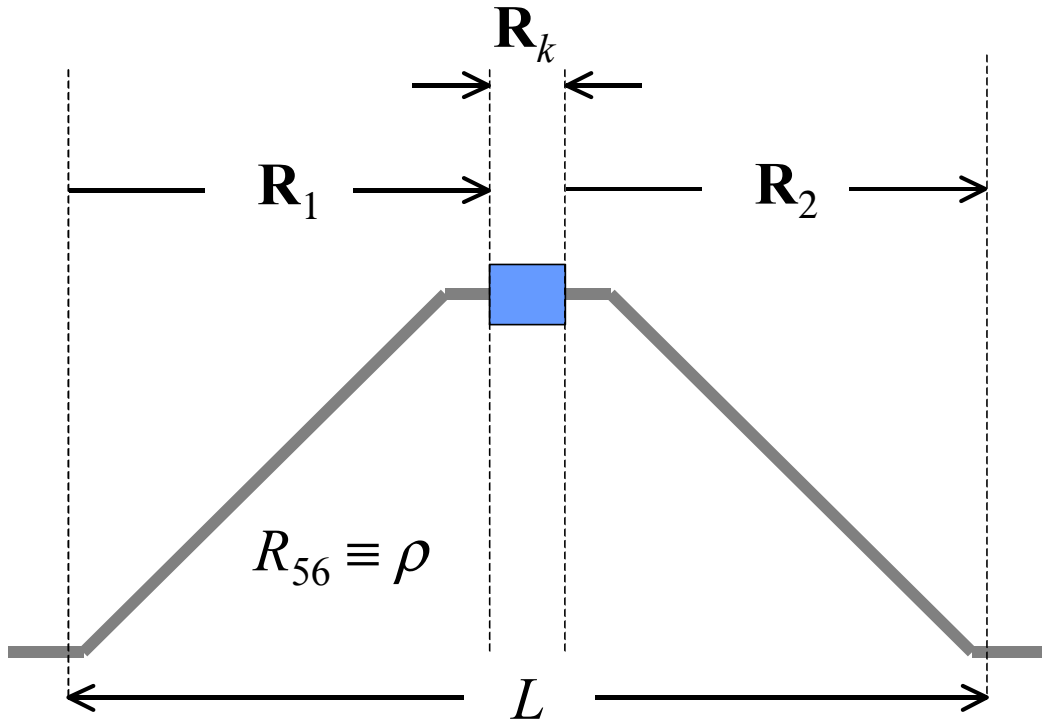
$$\delta \approx \frac{eV_0}{aE_0} x = kx, \quad \Delta x' \approx \frac{eV_0}{aE_0} z = kz$$

The transfer matrix of this thin-lens cavity is

$$\mathbf{R}_k = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & k & 0 \\ 0 & 0 & 1 & 0 \\ k & 0 & 0 & 1 \end{bmatrix},$$

which *looks like a thin-lens skew quad*, but here we consider the space (x, x', z, δ) .

Now place this cavity in a chicane...



$$\mathbf{R} = \mathbf{R}_2 \mathbf{R}_k \mathbf{R}_1$$

$$\mathbf{R}_1 = \begin{bmatrix} 1 & L/2 & 0 & \eta \\ 0 & 1 & 0 & 0 \\ 0 & \eta & 1 & \rho/2 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$\mathbf{R}_2 = \begin{bmatrix} 1 & L/2 & 0 & -\eta \\ 0 & 1 & 0 & 0 \\ 0 & -\eta & 1 & \rho/2 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$\mathbf{R} = \begin{bmatrix} 1 + \eta k & L & kL/2 & k\left(\frac{\rho L}{4} - \eta^2\right) \\ 0 & 1 - \eta k & k & k\rho/2 \\ k\rho/2 & k\left(\frac{\rho L}{4} - \eta^2\right) & 1 + \eta k & \rho \\ k & kL/2 & 0 & 1 - \eta k \end{bmatrix}$$

$$|\mathbf{A}| = |\mathbf{D}| = 1 - \eta^2 k^2, \quad |\mathbf{B}| = |\mathbf{C}| = \eta^2 k^2$$

Now work out $\lambda^2 \dots$

$$\mathbf{U} = \mathbf{Q}_x^{-1} \mathbf{A}^a \mathbf{B} \mathbf{Q}_z^{-1}$$

$$\lambda^2 = \text{tr}\{\mathbf{U}\mathbf{U}^T\} = 4 \text{ terms, or for } k = -\frac{1}{\eta} \dots$$

$$\lambda^2 = \frac{4(1 + \alpha_x^2)(1 + \alpha_z^2)}{k^2 \beta_x \beta_z} = \frac{4\sigma_{x'}^2 \sigma_\delta^2 \eta^2}{\varepsilon_{x_0} \varepsilon_{z_0}}.$$

Emittance are...

$$\varepsilon_x = \sqrt{\varepsilon_{z_0}^2 + 4\sigma_{x'}^2 \sigma_\delta^2 \eta^2} > \varepsilon_{z_0}$$

$$\varepsilon_z = \sqrt{\varepsilon_{x_0}^2 + 4\sigma_{x'}^2 \sigma_\delta^2 \eta^2} > \varepsilon_{x_0}$$

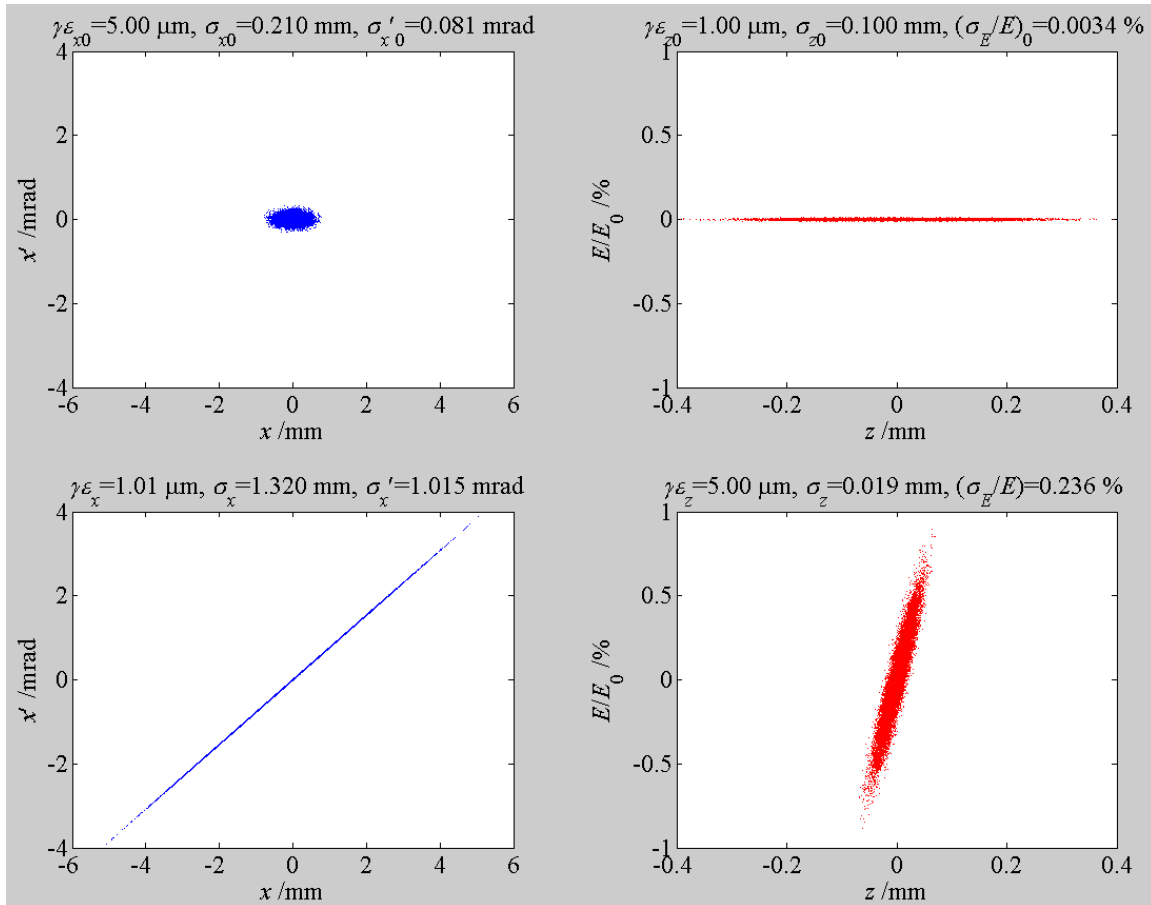
If $\varepsilon_{x_0} = \varepsilon_{z_0}$, then $\varepsilon_x = \varepsilon_z$ (i.e., always equal).

For example, take $\beta_x = 2.6$ m, $\sigma_z = 100$ μm ,
 $\sigma_E = 5$ keV, $\beta_z = 2.9$ m, $\alpha_x = \alpha_z = 0$, $E_0 =$
 150 MeV, $\eta = 100$ mm, $k = 10$ m^{-1} , $a = 1$
cm, $V_0 = 15$ MV...

$$\gamma\varepsilon_{x_0} = 5 \mu\text{m} \rightarrow \gamma\varepsilon_x = \gamma\varepsilon_{z_0} \sqrt{1+0.026} \approx 1 \mu\text{m}$$

$$\gamma\varepsilon_{z_0} = 1 \mu\text{m} \rightarrow \gamma\varepsilon_z = \gamma\varepsilon_{x_0} \sqrt{1+0.001} \approx 5 \mu\text{m}$$

Get nearly complete emittance exchange.

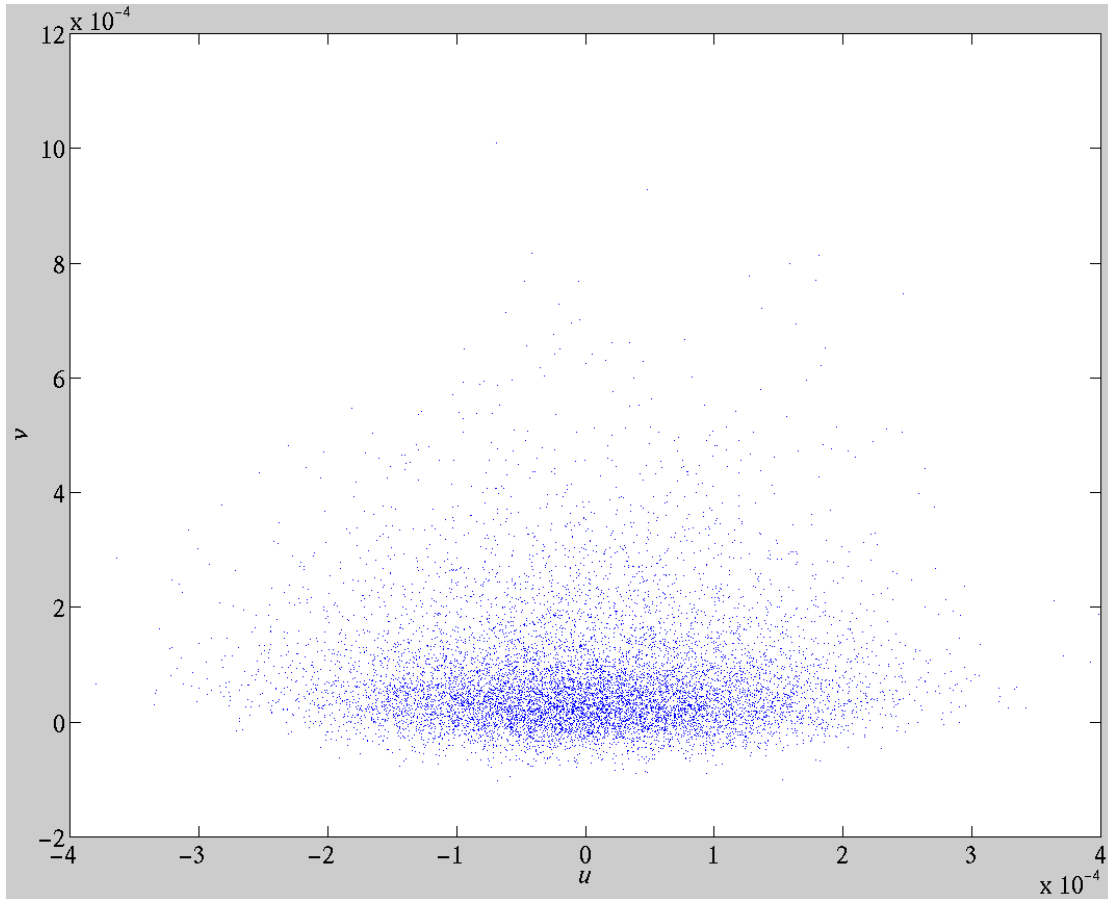


Bunch length for $k = -1/\eta$, and $\alpha_x = 0 \dots$

$$\sigma_z^2 = k^2 \varepsilon_{x_0} \left[\frac{\rho^2 \beta_x}{4} + \frac{1}{\beta_x} \left(\frac{\rho L}{4} - \frac{1}{k^2} \right)^2 \right] + \rho^2 \sigma_{\delta_0}^2$$

Bunch also typically compresses.

Second-order optics (T_{166}) can be significant, but use small β_x and/or large η (small k) for control...



➔ $\beta_x = 10 \text{ m}$, $\eta = 50 \text{ mm} \rightarrow \sigma_E/E \approx 0.8\%$

$\gamma \mathcal{E}_x \approx 3.1 \mu\text{m}$ (linear: $1 \mu\text{m}$).

$\gamma \mathcal{E}_z \approx 10 \mu\text{m}$ (linear: $5 \mu\text{m}$).

But, for $\beta_x = 2.6 \text{ m}$, $\eta = 100 \text{ mm} \rightarrow$
 $\sigma_E/E \approx 0.2\%$ get...

$\gamma \mathcal{E}_x \approx 1.07 \mu\text{m}$

$\gamma \mathcal{E}_z \approx 5.22 \mu\text{m}$

Tolerances...

$1 \cdot \sigma$ centroid jitter becomes $1 \cdot \sigma$ jitter, but in the other plane:

$$\begin{aligned} \langle x_0 \rangle = \sigma_{x0} & \rightarrow \langle z \rangle = \sigma_z, \quad \langle \delta \rangle = \sigma_\delta \\ \langle x'_0 \rangle = \sigma_{x'0} & \rightarrow \langle \delta \rangle \approx \sigma_\delta / 2 \\ \langle z_0 \rangle = \sigma_{z0} & \rightarrow \langle x \rangle = \sigma_x, \quad \langle x' \rangle = \sigma_{x'} \\ \langle \delta_0 \rangle = \sigma_{\delta 0} & \rightarrow \langle z \rangle = \sigma_z / 30 \end{aligned}$$

$$\begin{aligned} |\Delta V / V_0| < 0.5\% & \rightarrow |\Delta \mathcal{E} / \mathcal{E}_x| < 3\% \\ |\Delta \phi| < 0.3^\circ \text{ S-band} & \rightarrow |\langle x \rangle| < \sigma_x, \quad |\langle x' \rangle| < \sigma_{x'} \end{aligned}$$

$|\alpha_z| < 2.5$ (i.e., projected energy spread up to 3-times larger than intrinsic spread, for these parameters)

$$\rightarrow |\Delta \mathcal{E} / \mathcal{E}_x| < 10\%$$